



# Research on CO<sub>2</sub> EOR Technology and Application in China

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**Dr. XU TING**

**Petroleum Exploration & Production Institute of SINOPEC in China**

石油勘探开发研究院

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# OUTLINE

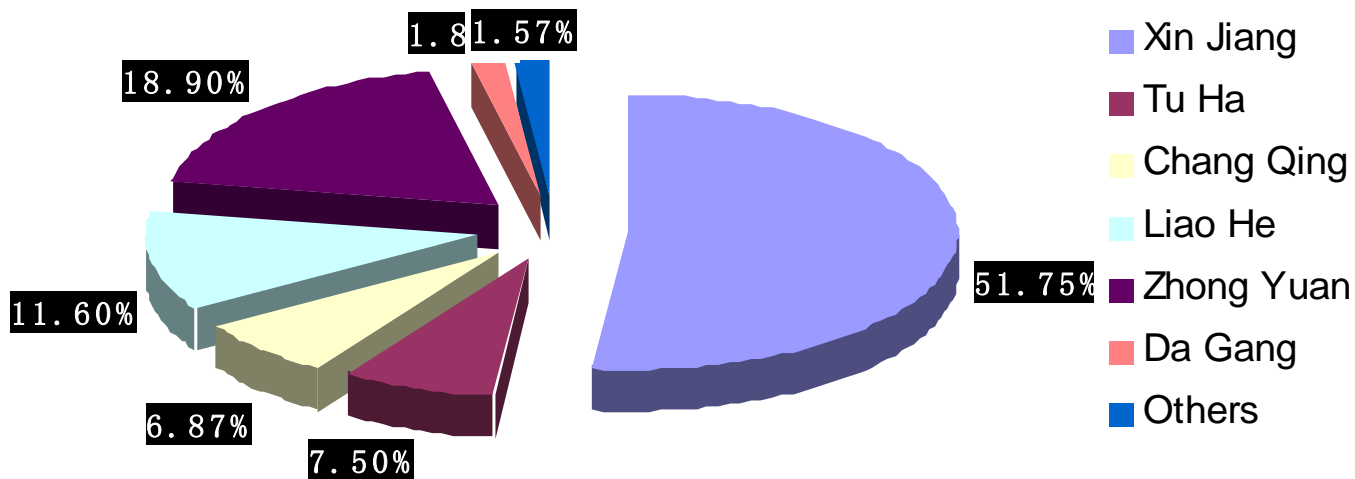
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- **General Introduction of Domestic CO<sub>2</sub> EOR Practice**
- **Issues in Laboratory Research and Solutions**
- **Issues in Field Implementation and Solutions**



# Domestic Technical Potential Distribution For CO<sub>2</sub> Miscible Flooding (2000)

Potential Evaluation for CO<sub>2</sub> Miscible Flooding Technology in China





# General Introduction of Domestic CO<sub>2</sub> EOR Practice

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**In 1963, firstly as main EOR technique, research on CO<sub>2</sub> EOR has been taken in DaQing oilfield. Then pilot projects have been put forward since 1966, 1969, 1985, 1991 and 1994.**

**In Jilin oilfield, with liquid CO<sub>2</sub> in Wanjinta CO<sub>2</sub> gas field , CO<sub>2</sub> huff & puff and foam fracturing have been operated in more than 100 wells.**

**In 1996, CO<sub>2</sub> huff & puff pilot projects in 48 wells were carried out in Fumin oilfield in Jiangsu Province.**



# General Introduction of Domestic CO<sub>2</sub> EOR Practice

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**In 2000, CO<sub>2</sub> huff & puff pilot projects in 16 wells were successfully fulfilled in Dongxin area of Shengli oilfield.**

**In 2002, CO<sub>2</sub> huff & puff were fulfilled after steam stimulation cycle in lots of blocks of Liaohe oilfield.**

**In 2007, CO<sub>2</sub> huff & puff were carried out in Deep heavy oil reservoir of Tuha oilfield and shallow heavy oil reservoir of Santanghu Basin.**



# General Introduction of Domestic CO<sub>2</sub> EOR Practice

Case 1

Maintaining minimum miscibility pressure, in **Fu 14 blocks of Jiangsu Province**, CO<sub>2</sub>-water alternating (WAG) injection project began in **late 1998**. After 6-cycle, water and gas ratio rise from 0.86:1 up to 2:1 and oil production were increased significantly. After water flooding, new oil-rich zone came into being.

Effect of increasing oil production in main producing wells of pilot area

井号	试验前		见效初期			峰值		累积增产油量 (t)
	产油量 (m <sup>3</sup> /d)	含水率 (%)	见效时间 (年.月.日)	产油量 (m <sup>3</sup> /d)	含水率 (%)	产油量 (m <sup>3</sup> /d)	含水率 (%)	
富 61	0.1	99.6	1999.2.28	1.7	91.7	13	52	2169.9
富 111	0.7	95	1999.7.27	2.8	82.4	11.4	60	1036.4
富 66A	1.1	90	2000.6.22	6.8	89.8	8.3	87	892.2
富 29	0	100	2000.6.10	2.9	87.2	6.4	75.7	288.4
富 70	0	100	2000.9.09	1.0	97.8	4.4	89.7	334.3



# General Introduction of Domestic CO<sub>2</sub> EOR Practice

## Case II

Since March 2000, CO<sub>2</sub> huff & puff pilot projects have been carried out in selected 16 wells of different blocks and strata of **Dongxin area** with 70% successful operating rate and  $1.6755 \times 10^4$ t of cumulative increasing oil production.

东辛采油厂 CO<sub>2</sub> 吞吐工艺效果统计表(2001.11)

序号	井号	生产层位	注入 CO <sub>2</sub> 总量 /t	累计增油 /t	增加采出程度 / %	换油率 t/tco <sub>2</sub>	分类
1	辛 50 - 斜 59	S <sub>2</sub> <sup>6</sup>	200	4762	40.79	23.81	I
2	辛 139 - 1	S <sub>3</sub> 中 <sup>1</sup>	50	3504.4	8.66	70.09	I
3	辛 17 - 22	S <sub>2</sub> <sup>4</sup>	150	2835.7	3.66	18.9	I
4	营 13 - 斜 113	S <sub>2</sub> <sup>4</sup>	50	1597.4	1.03	31.95	I
5	辛 48 - 斜 25	S <sub>2</sub> <sup>4,5</sup>	60	906.4	1.21	15.11	II
6	辛 37 - 斜 40	S <sub>2</sub> 稳	35	876.5	1.77	25.04	II
7	辛 34 - 45	S <sub>2</sub> <sup>9</sup>	80	445.1	1.23	5.56	II
8	辛 47 - 斜 54	S <sub>2</sub> <sup>2-4</sup>	80	429.7		5.37	II
9	辛 25 - 斜 14	S <sub>2</sub> <sup>2-4</sup>	50	368.3		7.34	III
10	辛 50 - 斜 43	S <sub>2</sub> <sup>6</sup>	50	213.1		4.26	III
11	辛 6 - 斜 30	S <sub>2</sub> <sup>8-9</sup>	80	173.8		2.17	III
12	辛 69 - 斜 7	S <sub>2</sub> <sup>1</sup>	70	148		2.11	III
13	辛 6 - 斜 47	S <sub>1</sub> <sup>4</sup>	15	115.5		7.7	III
14	营斜 591	S <sub>2</sub> 稳 - S <sub>3</sub>	60	22.2		0.37	III
15	营 87 - 50	S <sub>2</sub> <sup>4</sup>	50	12		0.24	III
16	营 2 - 斜 25	S <sub>3</sub>	100	3.6		0.036	III
合计			1180	16375.9		13.88	

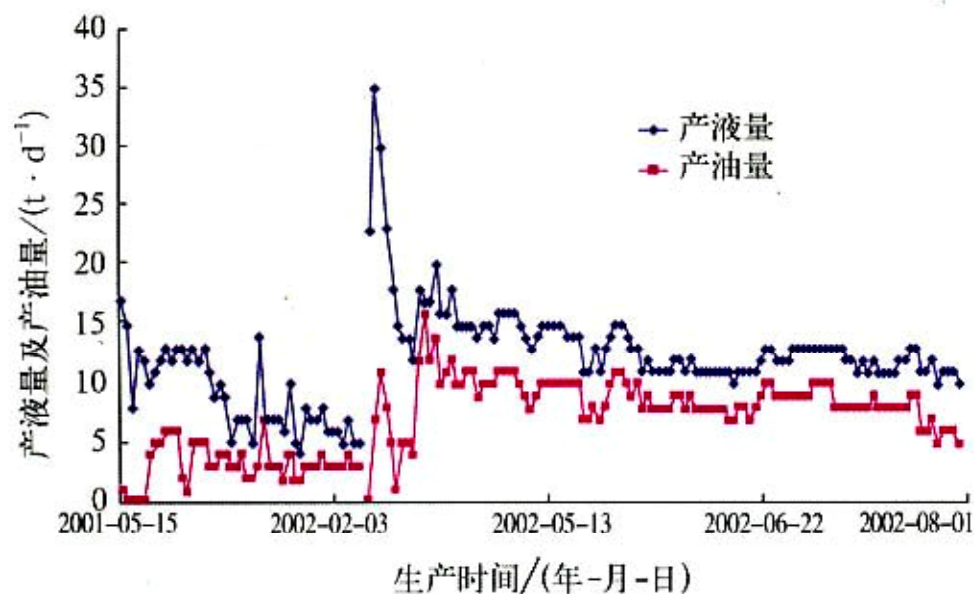


# General Introduction of Domestic CO<sub>2</sub> EOR Practice

## Case III

**Jin 45-25-193 Well** was put into operation in March 1998 and in 2002 six cycles were finished. Before CO<sub>2</sub> huff & puff, daily oil production was 2t/d and steam stimulation has attained to the economic limit.

In April 2002, after six cycles of steam stimulation, **CO<sub>2</sub> huff & puff** was carried out with **16t/d of initial daily oil production**.







# OUTLINE

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- **General Introduction of Domestic CO<sub>2</sub> EOR Practice**
- **Issues in Laboratory Research and Solutions**
- **Issues in Field Implementation and Solutions**



## Issues in Laboratory Research and Solutions

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**In China, most of oil reservoir is of continental deposit and non-marine origin of hydrocarbon. Domestic crude oil is of high viscosity, high content of wax and resin, high freezing point, the high minimum miscibility pressure (MMP) of CO<sub>2</sub>-crude oil.**



# Solution I

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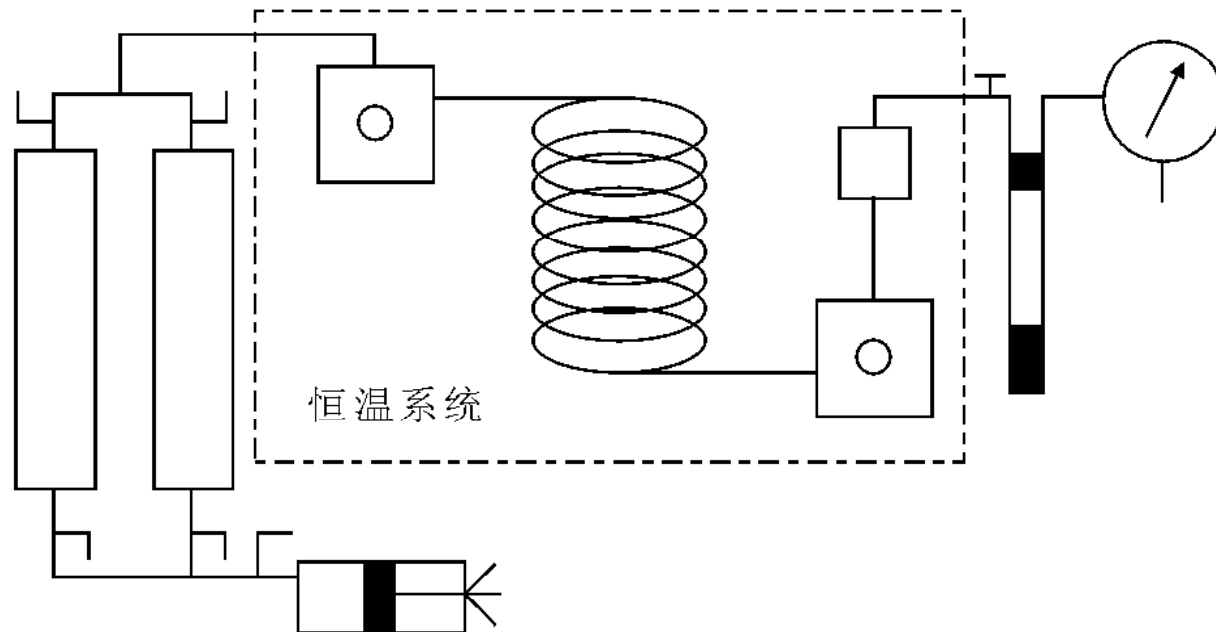
## Research on physical chemistry theory in CO<sub>2</sub> miscible recovery process:

- Research on phase characteristics and influencing factors of CO<sub>2</sub>-crude oil in CO<sub>2</sub> miscible recovery process.
- Searching for multi-component phase state characterization of CO<sub>2</sub> and complex hydrocarbons.
- Study on oil physical and chemical properties, pressure/temperature sensitivity, light component extraction and heavy components deposition in CO<sub>2</sub> miscible recovery process.
- Developing and establishing phase-state theory in equilibrium state process, in dynamic process and in porous media (micro scale) for improvement of CO<sub>2</sub> state equation suited to domestic crude oil.



## Slim Tube Experiment for CO<sub>2</sub>-Crude oil

Slim tube device is an effective one-dimensional flowing experiment model simulating dynamic miscibility process of multi-contacts in CO<sub>2</sub> injection process and determining minimum miscibility pressure (MMP).

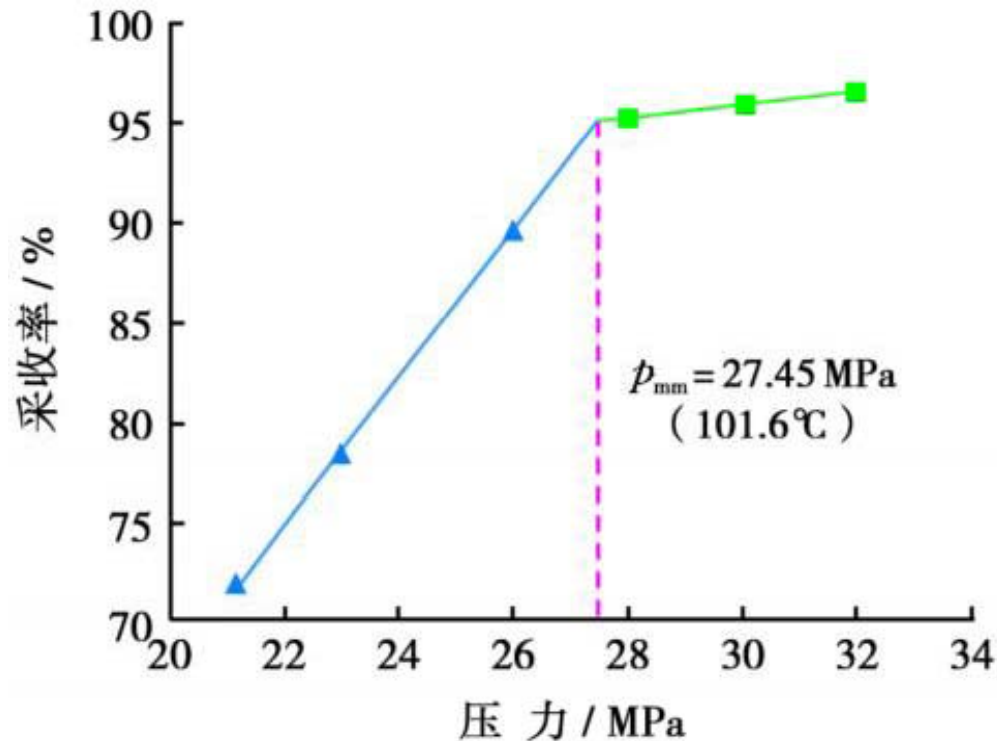




# Slim Tube Experiment for CO<sub>2</sub>-Crude oil

## MMP acquired from slim tube experiment

Criteria for miscible flooding is 80% of oil recovery as gas breaks through or 90%~95% of ultimate recovery.



Ultimate oil recovery with different pressure



# PVT Multi-Contact Tests for CO<sub>2</sub>-Crude oil

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Multi-contact tests could be divided into contacts as move forward and backward, respectively modeling crude oil phase state and composition of front and back edge in contact with CO<sub>2</sub>.

## Case:

**T=101.6°C**

**P=21.2MPa(Reservoir pressure) , 30MPa(>MMP 27.45MPa)**

**Contacts forward: 4 times**

**Contacts backward: 6 times**

**All in non-miscible and miscible process**



## Dynamic change of gas and liquid composition in multi-contact tests

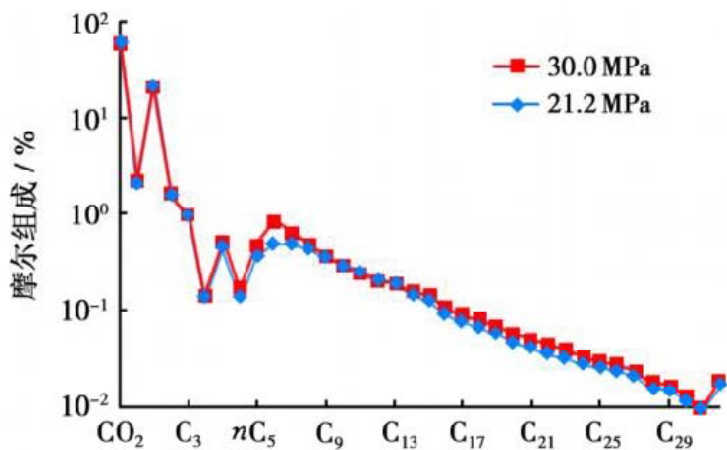
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### High extraction potent of CO<sub>2</sub>-crude oil

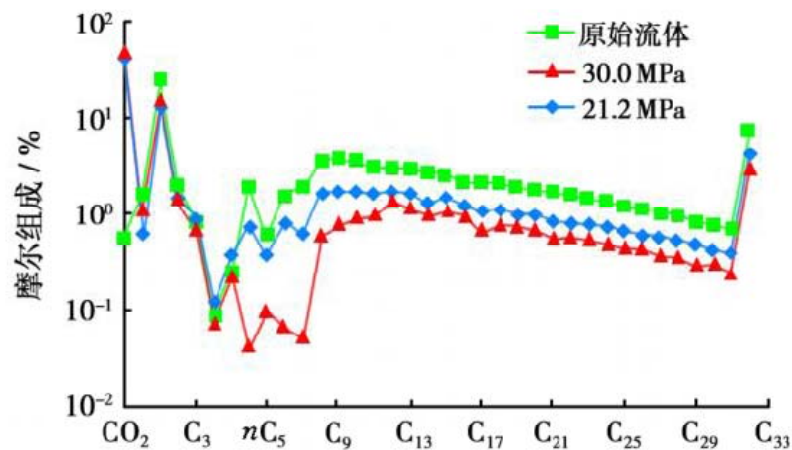
CO<sub>2</sub> flooding can vaporize not only the light hydrocarbon less than C<sub>11</sub>, but even the heavy hydrocarbon components such as C<sub>32</sub>.



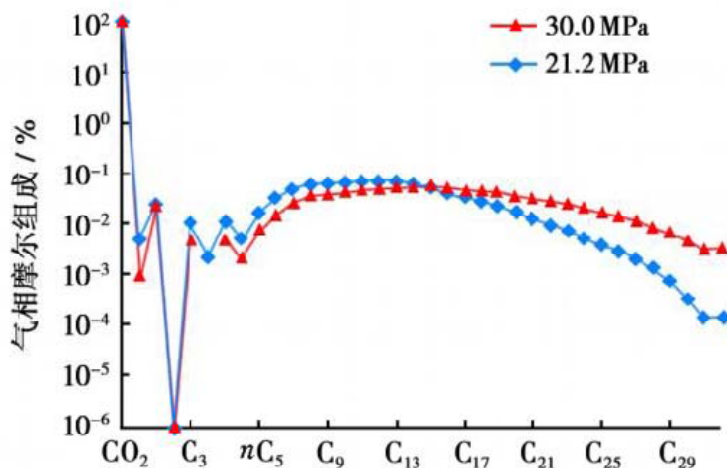
# Pressure Effect on Phase Components of Multi-Contact tests



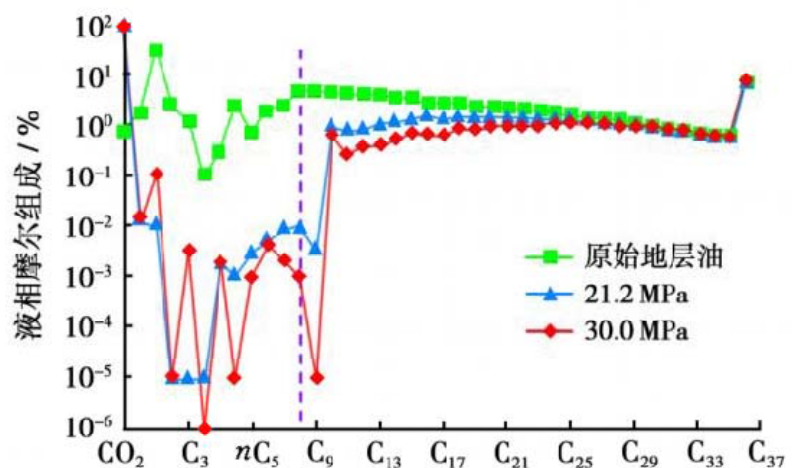
(a) 压力对向前接触过程中气相组分的影响



(b) 压力对向前接触过程中液相组分的影响



(c) 压力对向后接触过程中气相组分的影响



(d) 压力对向后接触过程中液相组分的影响





# Pressure Effect on Phase Components of Multi-Contact tests

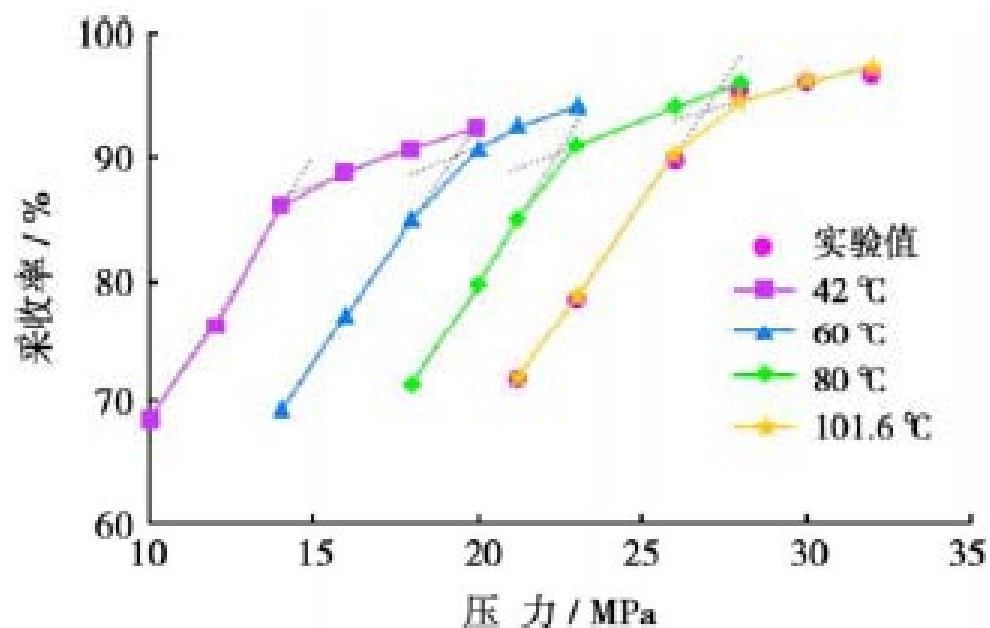
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Higher pressure is growing, greater CO<sub>2</sub> vaporization is, higher content of middle components is in gas phase and lower content of middle components is in liquid phase。



# Temperature Effect on MMP

Temperature impacts on MMP greatly. Lower temperature is, lower MMP is.





## Effect of contents of N<sub>2</sub> and CH<sub>4</sub> in CO<sub>2</sub> on MMP

With contents of CH<sub>4</sub> and N<sub>2</sub> increasing, MMP of CO<sub>2</sub>-crude oil increases. On the same content of N<sub>2</sub> and CH<sub>4</sub>, N<sub>2</sub> impacts on MMP more greatly than CH<sub>4</sub> does.

	MMP /MPa		
Content /%	10	20	30
N <sub>2</sub>	35.8	41.2	46.3
CH <sub>4</sub>	29.45	32.3	35.48



# Heavy Hydrocarbon Components Deposition in CO<sub>2</sub> Miscible Flooding Process

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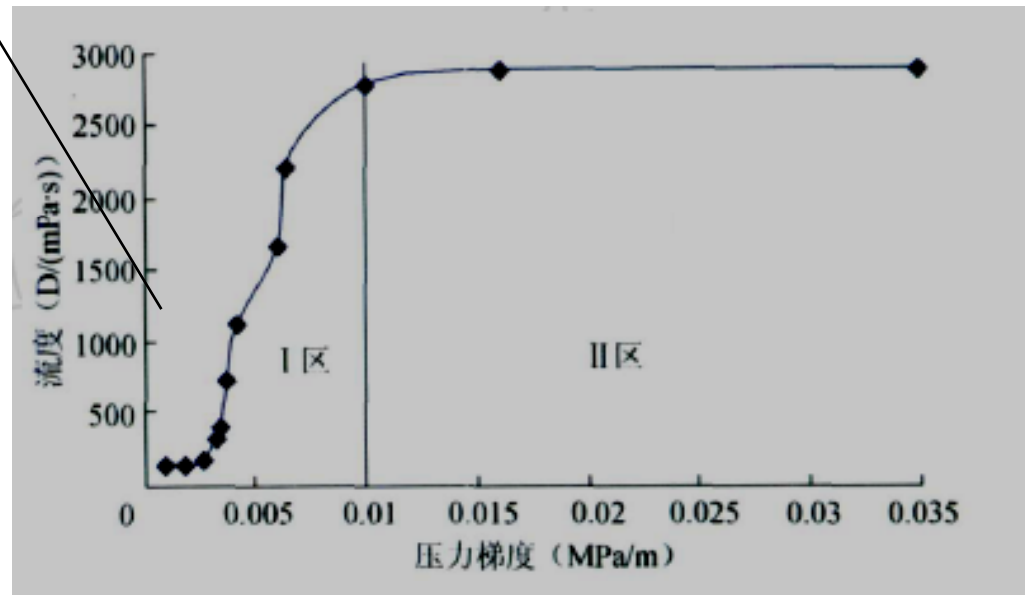
For high content of wax and asphaltene in heavy oil reservoir, CO<sub>2</sub> stimulation process makes solid of wax and asphaltene deposit and formation damaged again. So it is necessary to study mechanism of solid phase precipitation to enhance oil recovery for CO<sub>2</sub> stimulation technique.



## Setting Up Crude Oil Component Model Containing Asphaltenes in CO<sub>2</sub> Injection Process

In computation of the model, solution for non-newtonian fluid as following chart:

Asphaltene flocculates to be network structure, making crude oil flow slowly. With the pressure gradient increasing, network structure collapse, the other components of crude oil could be released gradually, flowing of crude oil shifts from non-Newtonian pattern to Newtonian pattern.



Relationship between pressure gradient and mobility as bituminous oil flowing in porous media.



## Effect of Asphaltene Deposition on Oil Recovery in CO<sub>2</sub> Injection Process

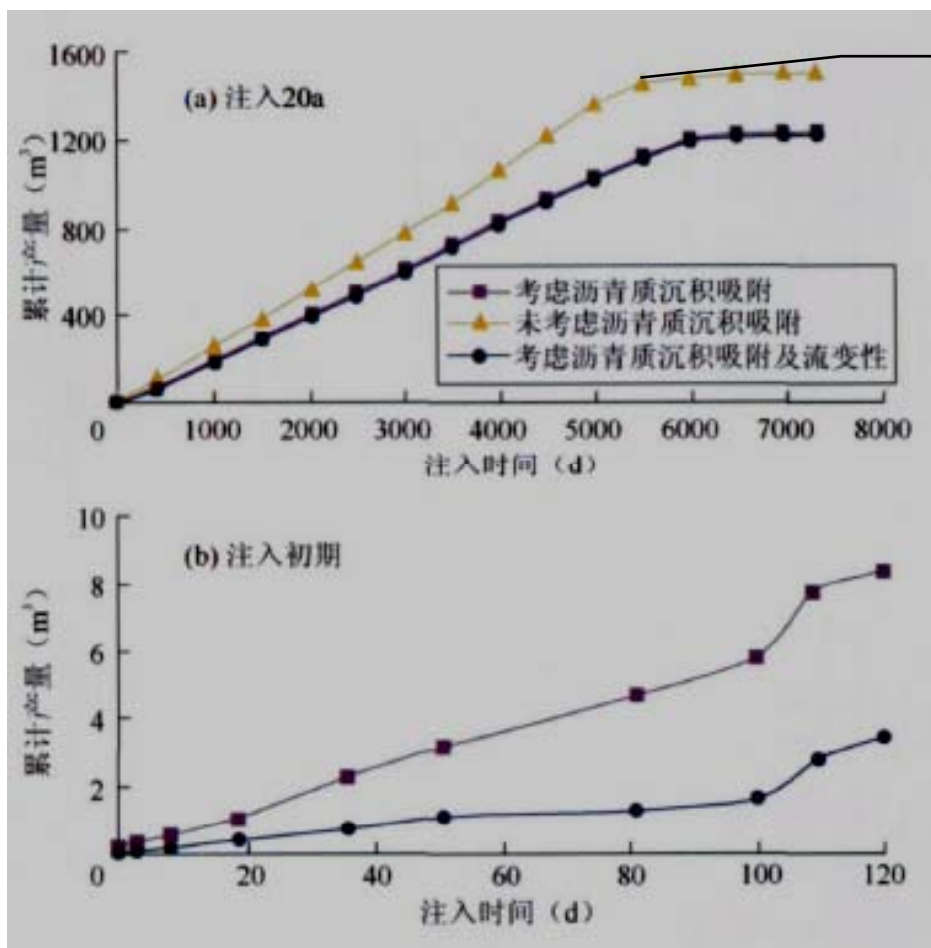
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Experiment results from CO<sub>2</sub> long model displacement test are compared with numerical model results.

Core No.	Core Length /cm	Differential Pressure /MPa	Recovery from Experiment /%	Recovery from New Numerical Model /%	Recovery from Classic Component Model /%
1	43.16	5	59.76	58.47	63.28
2	42.85	5	64.38	64.12	67.85
3	45.82	5	78.07	80.33	82.77
4	43.16	10	79.24	82.04	84.32



# Effect of Asphaltene Deposition on Cumulative Production in CO<sub>2</sub> Injection Process



Not considering adsorption of asphaltene deposition, CO<sub>2</sub> breaks through in production wells much earlier than real case considering asphaltene deposition and cumulative oil production is more than the one considering asphaltene deposition .



# Solution II

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## Research on flowing mechanics in CO<sub>2</sub> flooding process:

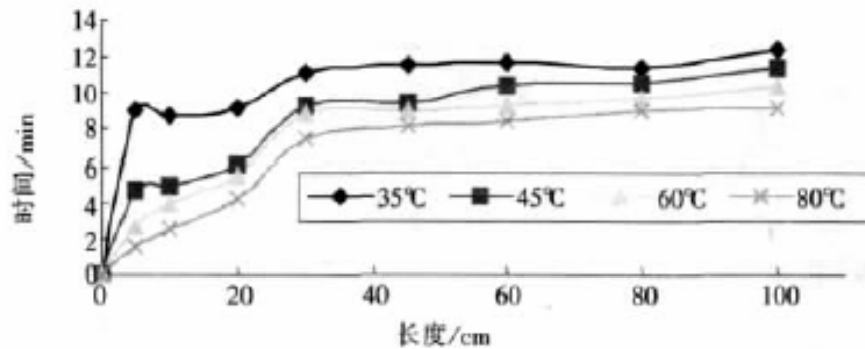
- Study on dispersion and diffusion theory in CO<sub>2</sub> Injection process
- Rheology of formation fluid in CO<sub>2</sub> injection process
- Research on complex flowing mechanism of CO<sub>2</sub>, oil, brine and multi-phase mixture in heterogeneous reservoir with macro- and microscopic simulating experiment under HPHT
- Integrated phase-state experiments with physical simulating experiments, multi-phase multi-component non-linear numerical simulation theory and method should be developed



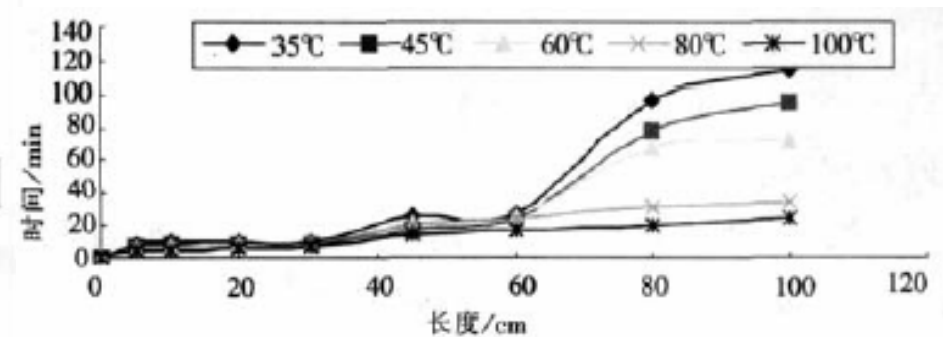


# CO<sub>2</sub> Diffusion in Porous Media

CO<sub>2</sub> diffuse faster in porous media filled with brine under high-temperature than the one unfilled with brine. At 60cm ~ 80cm near the outlet, due to CO<sub>2</sub> breakthrough, pressure on outlet fluctuates, equilibrium time extends correspondingly.



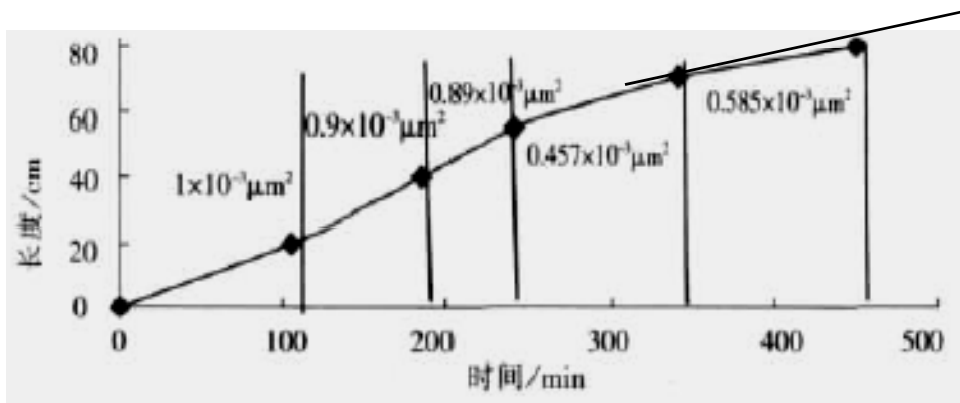
Relation between CO<sub>2</sub> diffusion equilibrium time and distance of core unfilled with brine



Relation between CO<sub>2</sub> diffusion equilibrium time and distance of core filled with brine



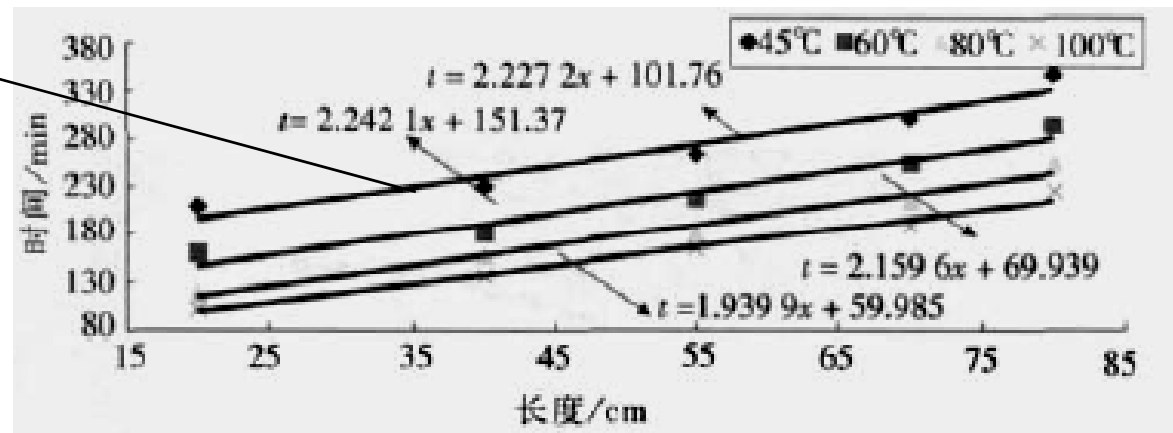
# Effect of Permeability and Temperature on CO<sub>2</sub> Diffusion



Effect of permeability on equilibrium time is greater than temperature does.

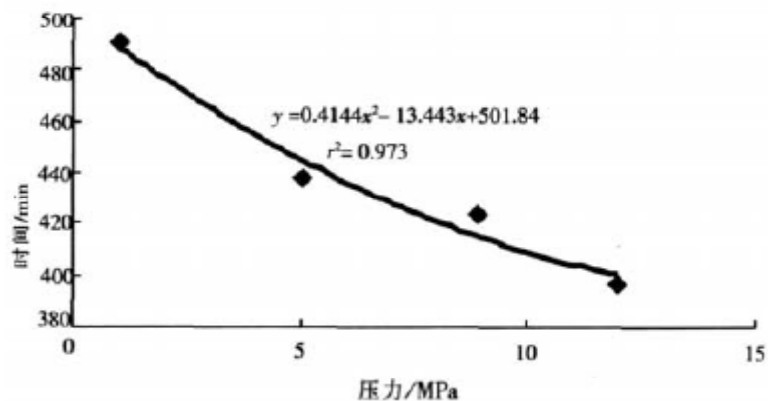
Capillary pressure increases as permeability is decreasing. The impact of much flowing resistance of CO<sub>2</sub> on equilibrium time is greater than temperature does.

As temperature is increasing from 45°C to 100°C, viscosity of brine decreases to 1/3 of original viscosity.

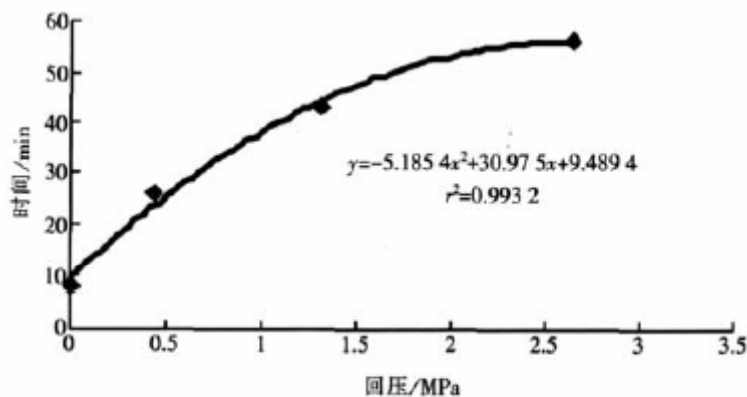




# Effect of Inlet Pressure and Back Pressure on CO<sub>2</sub> Diffusion



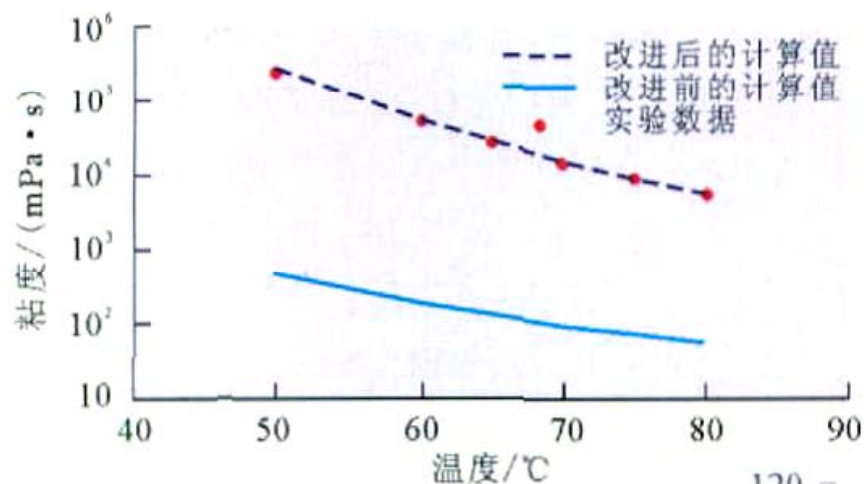
With **inlet pressure** increasing, diffusion equilibrium time starts to reduce rapidly, then reduces slowly by slowly.



With **back pressure** increasing, CO<sub>2</sub> moving resistance increases correspondingly.

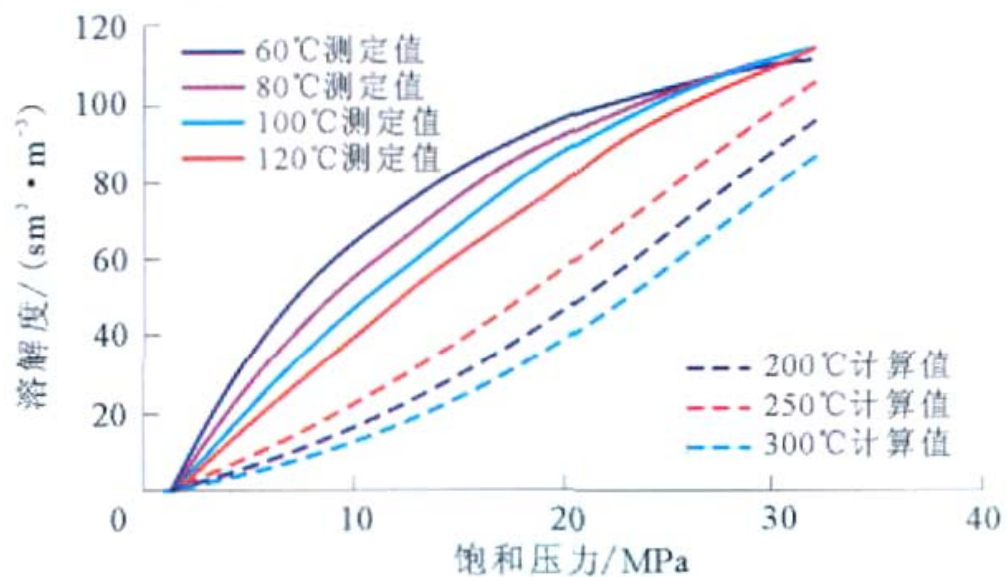


# Effect of CO<sub>2</sub> on Reducing Viscosity of Extra-Heavy Oil



Viscosity-temperature curve of Zheng 411 extra-heavy oil

CO<sub>2</sub> solubility\_ saturation pressure on different temperature





# Effect of CO<sub>2</sub> on Reducing Viscosity of Extra-Heavy Oil

Volume factors of extra-heavy oil dissolved CO<sub>2</sub> on different solubility of CO<sub>2</sub> and temperature

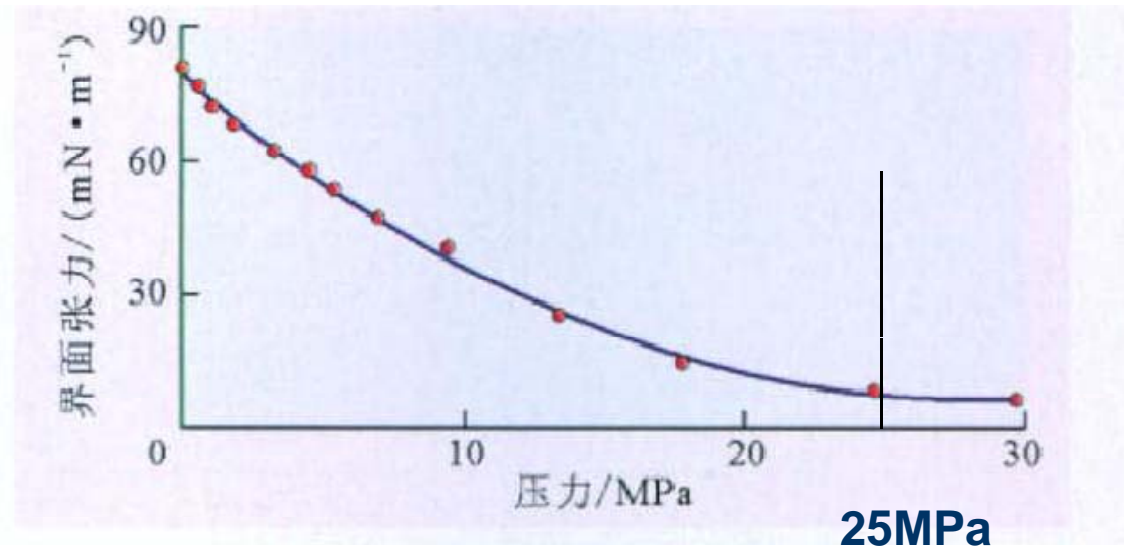
CO <sub>2</sub> 的溶解度 / (m <sup>3</sup> · m <sup>-3</sup> )	体 积 系 数 / (m <sup>3</sup> · m <sup>-3</sup> )			
	60 ℃	80 ℃	100 ℃	120 ℃
1	1.011	1.014	1.020	1.022
5	1.022	1.026	1.029	1.034
10	1.033	1.036	1.041	1.044
20	1.061	1.066	1.071	1.075
30	1.091	1.097	1.099	1.107
40	1.121	1.125	1.131	1.139
50	1.142	1.145	1.149	1.155
60	1.161	1.167	1.171	1.175
70	1.185	1.191	1.198	1.201
80	1.221	1.225	1.228	1.231
90	1.248	1.255	1.261	1.265
100	1.281	1.285	1.288	1.295
110	1.288	1.295	1.302	1.311

Viscosity of extra-heavy oil dissolved CO<sub>2</sub> on different solubility of CO<sub>2</sub> and temperature

CO <sub>2</sub> 的溶解度 / (m <sup>3</sup> · m <sup>-3</sup> )	粘 度 / (mPa · s)			
	60 ℃	80 ℃	100 ℃	120 ℃
1	55 279	6 167	1 382	467
5	25 481	3 524	887	311
10	13 658	2 146	574	207
20	5 789	861	285	113
30	3 005	516	175	75
40	1 554	356	105	47
50	1 015	238	75	37
60	760	175	63	29
70	480	120	46	25
80	413	95	38	19
90	312	80	29	16
100	231	62	27	13
110	198	53	21	10



# Effect of CO<sub>2</sub> on Reducing Viscosity of Extra-Heavy Oil



Interfacial tension of extra-heavy oil dissolved CO<sub>2</sub>



# Research on Complex Flowing Mechanism of CO<sub>2</sub>, Oil, Brine and Multi-phase Mixture through Macroscopic Simulating Experiment

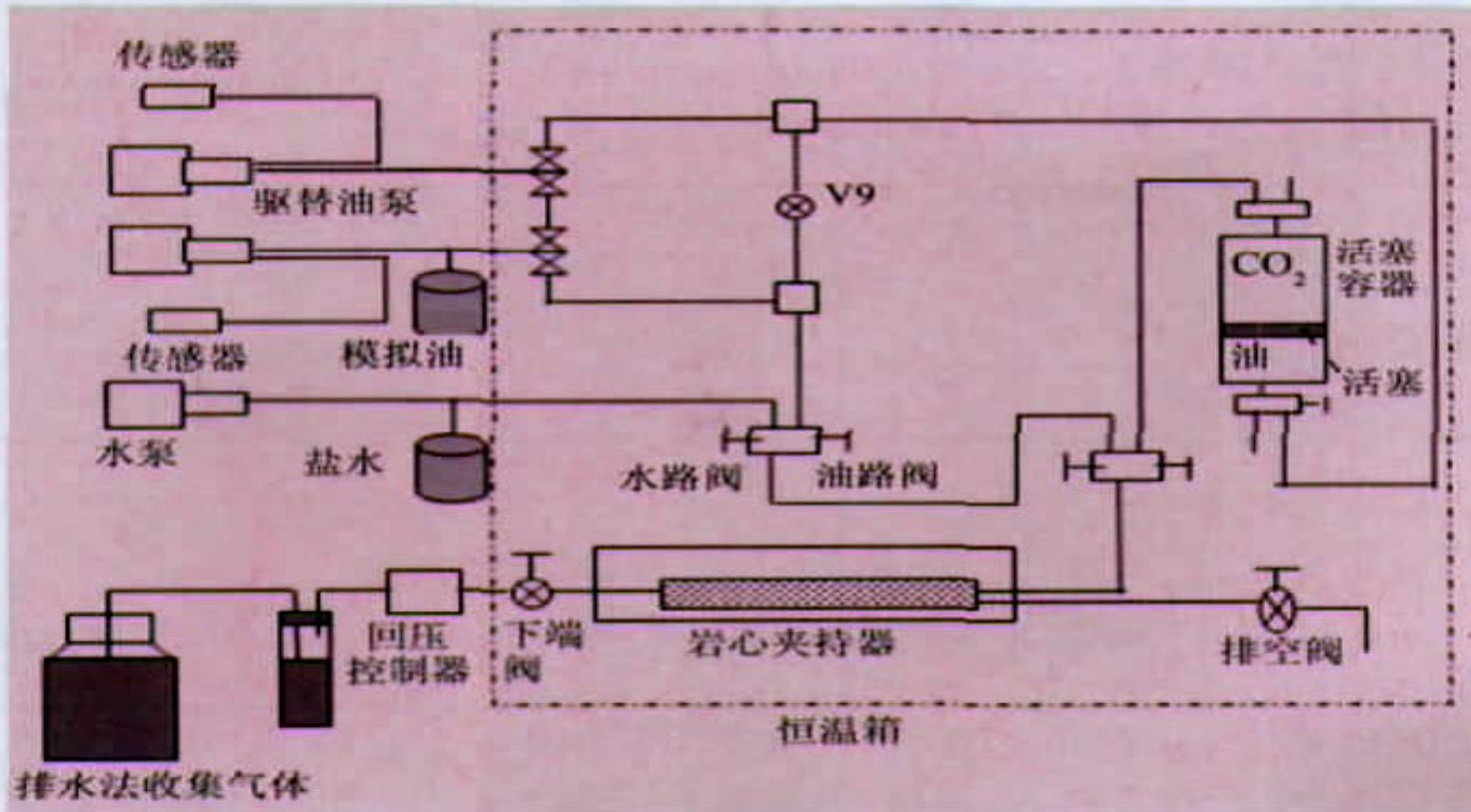
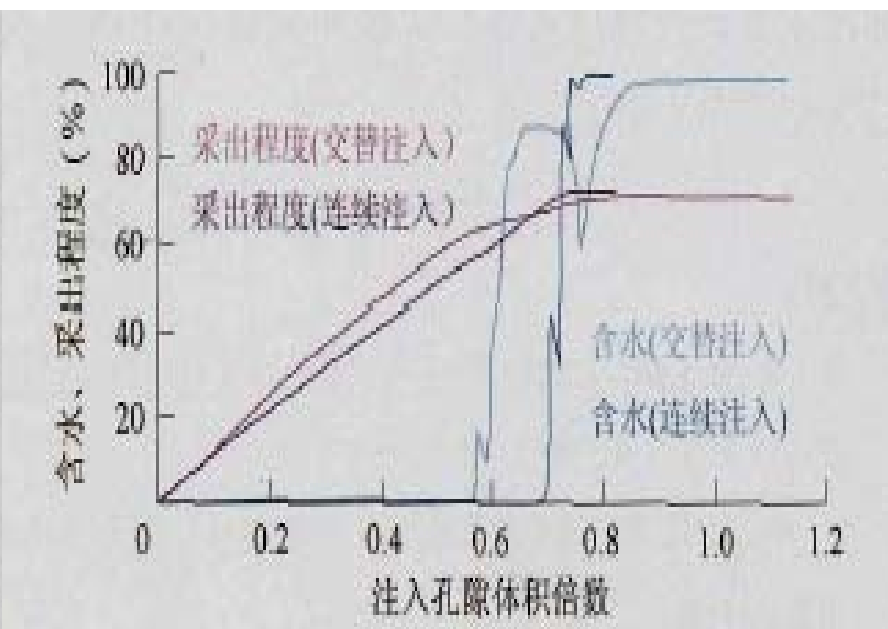
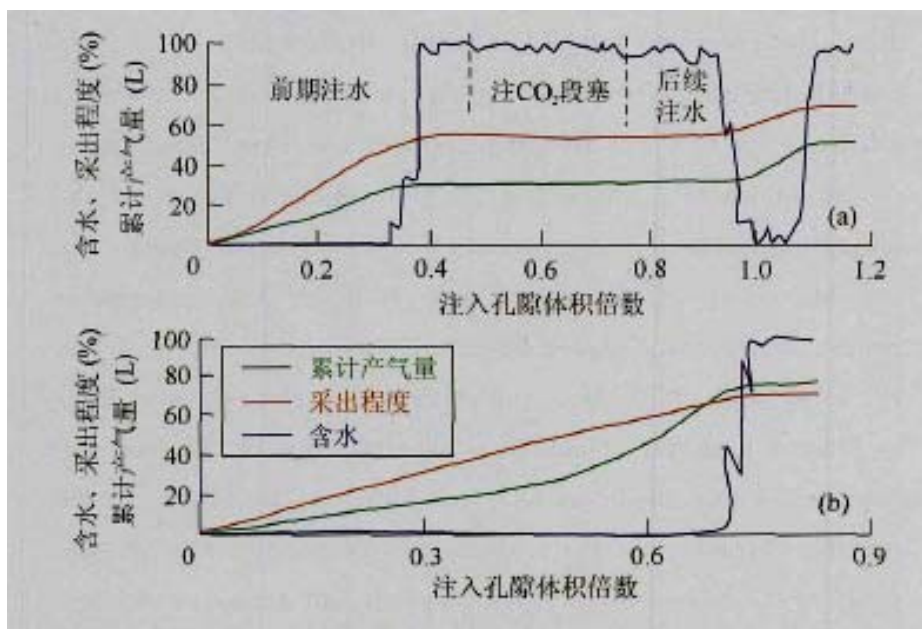


图 1 CO<sub>2</sub> 驱替实验流程图

Fig. 1 Flowchart of CO<sub>2</sub> flooding test



# Long-Core Physical Simulating Experiment Results



Enhanced oil recovery of CO<sub>2</sub> injection in water-free period is greater than the one in 99% of water cut.

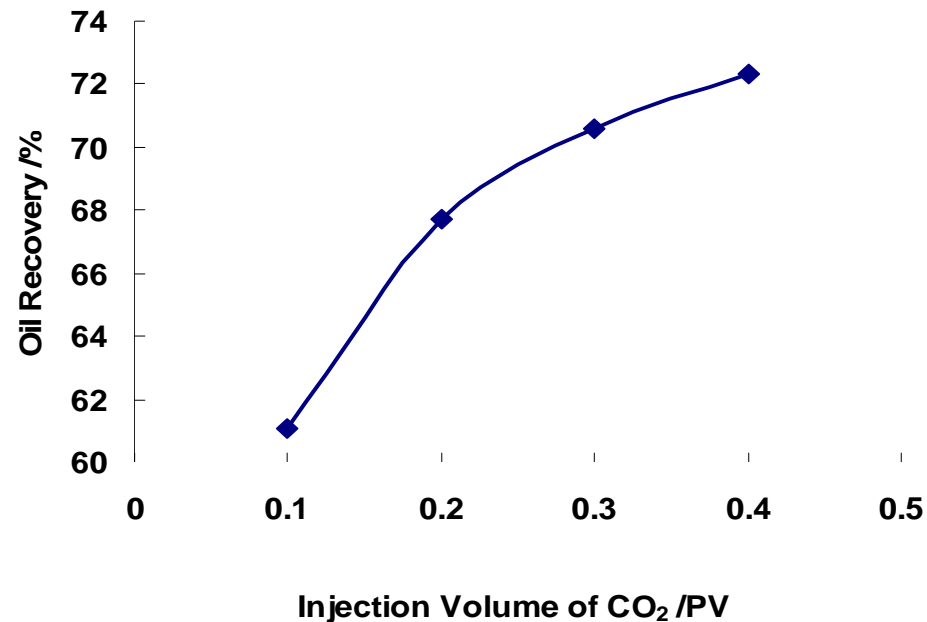
Enhanced oil recovery of 0.3 PV CO<sub>2</sub> of WAG is greater than continuous injection (gas-water ratio is 1:1)





# Long-Core Physical Simulating Experiment Results

Considering CO<sub>2</sub> channeling and leaking from injection equipment, CO<sub>2</sub> optimal injection volume is 0.25PV.





# Long-Core Physical Simulating Experiment Results

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## Suggestion:

On **CO<sub>2</sub> miscible flooding conditions**, in the heterogeneous strata, water alternating CO<sub>2</sub> injection control gas channeling effectively. Optimization of the amount of CO<sub>2</sub> should be 0.25PV.

On **CO<sub>2</sub> non-miscible flooding conditions**, slug size of CO<sub>2</sub> and reservoir pressure are most key factors to impact on CO<sub>2</sub> flooding. Furthermore afflux of CO<sub>2</sub> is also important to the effect of CO<sub>2</sub> flooding. The Effect of alternating injection and gas-water ratio is minor than above factors.



# CO<sub>2</sub> Flooding Experiment on Microscopic Model

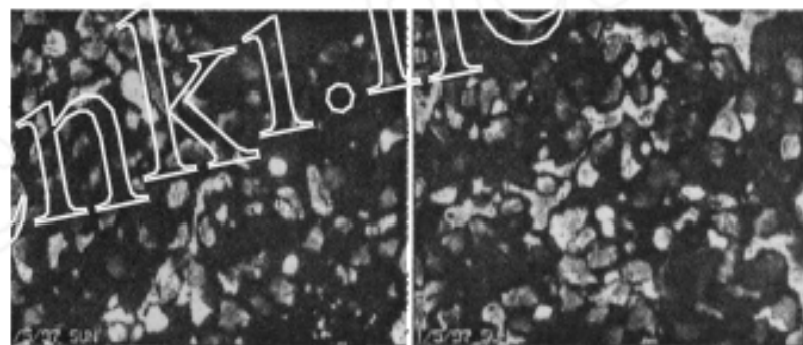
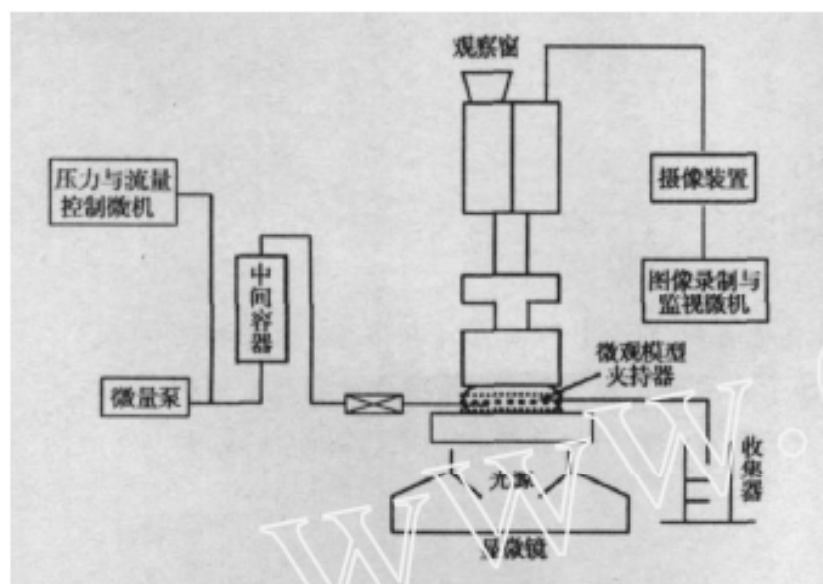


图2 水驱

图3 注入就地CO<sub>2</sub>体系

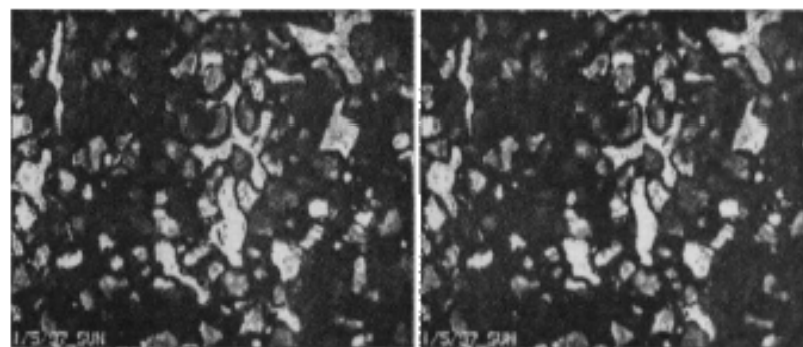
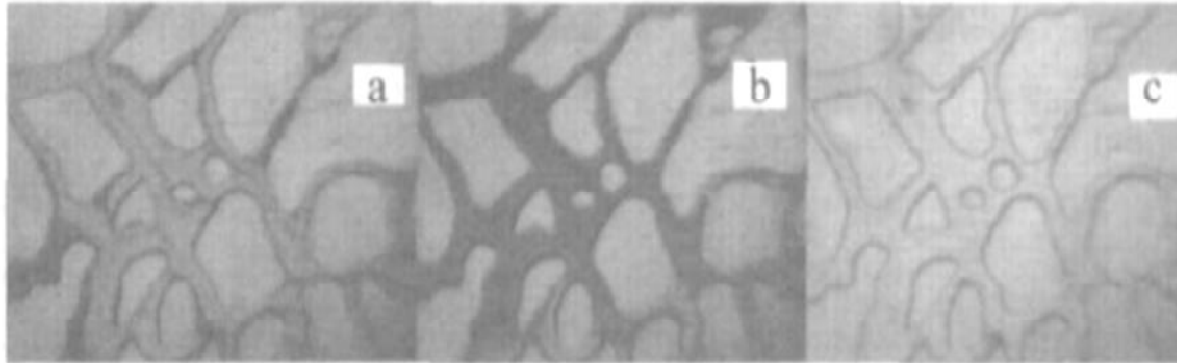


图4 注入体系后 30 min

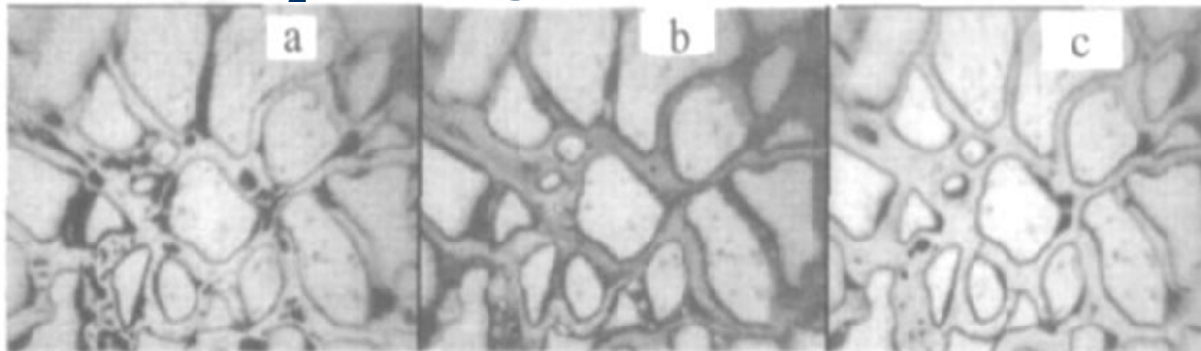
图5 注入体系后 2 h



# CO<sub>2</sub> Flooding Experiment on Microscopic Model



Microgram of enhanced oil recovery of CO<sub>2</sub> flooding in water-free period



Microgram of enhanced oil recovery of water-CO<sub>2</sub> alternating flooding

In heterogeneous strata, WAG increases sweep efficiency, postponing CO<sub>2</sub> breakthrough from outlet. But water could shelter oil flowing in pore-throat structure making displacement efficiency deteriorate.



# OUTLINE

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- **General Introduction of Domestic CO<sub>2</sub> EOR Practice**
- **Issues in Laboratory Research and Solutions**
- **Issues in Field Implementation and Solutions**



# Issues of Field Implementation

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- **Applicability of Reservoir and Injection Pattern**
- **Premature Gas Channeling and Low Sweep Efficiency**
- **Corrosion**
- **CO<sub>2</sub> Source**



# Solution I

**Set up CO<sub>2</sub> injection screening criteria suitable to characterization of domestic oil reservoir:**

<b>Displacement Type</b>	<b>Relative Density of Crude oil</b>	<b>Reservoir Depth /m</b>	<b>Oil Viscosity /mPa.s</b>
<b>CO<sub>2</sub> Miscible Flooding</b>	<b>&lt;0.825</b>	<b>&gt;762</b>	<b>&lt;10</b>
	<b>0.825-0.865</b>	<b>&gt;853</b>	<b>&lt;10</b>
	<b>0.865-0.887</b>	<b>&gt;1006</b>	<b>&lt;10</b>
	<b>0.887-0.922</b>	<b>&gt;1219</b>	<b>&lt;10</b>
<b>CO<sub>2</sub> Non-Miscible Flooding</b>	<b>0.92-0.98</b>	<b>549</b>	<b>&lt;600</b>



# Solution I

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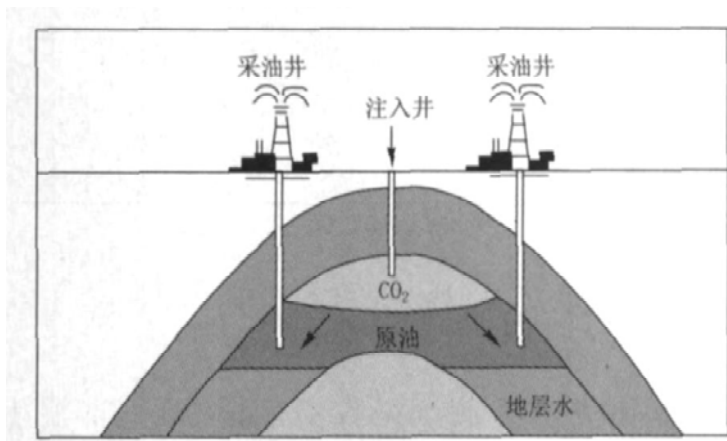
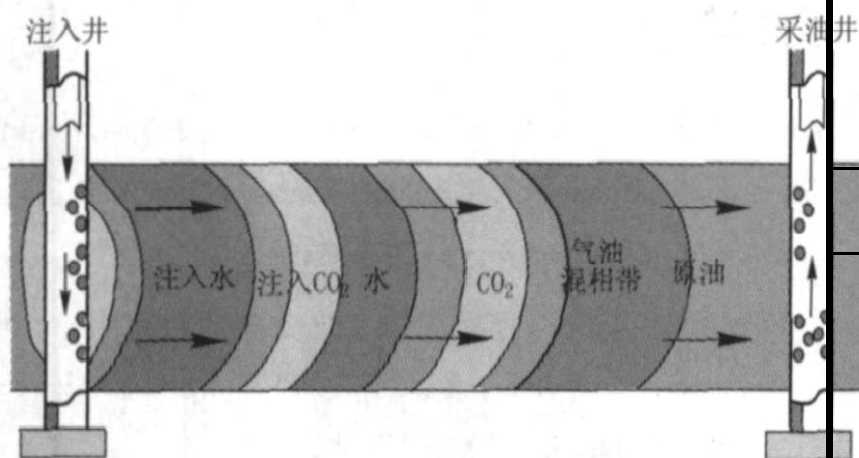
## Domestic oil reservoir suitable to miscible flooding:

- Low permeability reservoir with poor water flooding
- Completely depleted sandstone reservoir after water flooding
- Light hydrocarbon deep reservoir approaching production economic limits
- Exploitation of salt dome reservoir by CO<sub>2</sub> gravity miscible flooding





# Solution I



Displacement Type	Miscible flooding	Non-miscible flooding
Duration /a	<20	10
Project commencement	Before water flooding or after water flooding	After water flooding
Flooding mechanism	complex	easy
CO <sub>2</sub> circulation	unusable	usable
Potential for EOR	low	high
Potential for geological storage	low	high
Worldwide application	Commercial scale	Limited scale



# Solution I

**WAG is still the most important on-site development means.**

**Comparative analysis on different CO<sub>2</sub> injection process**

<b>Injection Process</b>	<b>Advantage</b>	<b>Disadvantage</b>	<b>Impacting factors</b>
<b>Continuous injection</b>	<b>High displacement efficiency, low MMP</b>	<b>Large quantity of CO<sub>2</sub>, earlier breakthrough, small sweep area</b>	<b>Injection rate, quantity of CO<sub>2</sub>, permeability and saturation of formation</b>
<b>WAG</b>	<b>High sweep efficiency, low CO<sub>2</sub> recovery</b>	<b>Water sheltering oil, oil bypassed and corrosion</b>	<b>Heterogeneous formation, wettability, relative parameter in WAG, permeability and fluid property etc.</b>
<b>CO<sub>2</sub> Huff and Puff</b>	<b>Low cost, high CO<sub>2</sub> utilization</b>	<b>Low oil recovery</b>	<b>Injection rate, cycle injection rate, shut-in time etc.</b>
<b>Drive by gravity</b>	<b>High oil recovery</b>	<b>Large quantity of CO<sub>2</sub>, reservoir with large dip</b>	<b>Injection rate, formation dip</b>
<b>SSWG</b>	<b>Large sweep area</b>	<b>Gravity overriding and corrosion</b>	<b>Non-homogeneity, wettability</b>



# Solution II

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**Combined with other EOR methods, mobility ratio could be improved:**

- ✓ **Thickening agent**
- ✓ **Foam alternating CO<sub>2</sub> injection**
- ✓ **Surfactant alternating CO<sub>2</sub> injection**

## **Intelligent completion technology:**

**With bottom-hole flowing control valve, recovery of CO<sub>2</sub> from production wells and afflux of CO<sub>2</sub> into injection wells could be controlled. Sweep efficiency is improved by reducing unnecessary circulation of CO<sub>2</sub> between pairs of wells.**



# Solution III

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## Corrosion theory



## Anti-corrosion measure

- ✓ corrosion resisting metal material
- ✓ corrosion resisting coat
- ✓ corrosion resisting nonmetal material
- ✓ corrosion inhibitor treatment



# Solution IV

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**Searching for CO<sub>2</sub> source and utilize industry exhaust gas:**

**Foreign Countries: CO<sub>2</sub> gas source and industry exhaust gas**

**China: CO<sub>2</sub> gas source is limited**



# Solution IV

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**CO<sub>2</sub> reservoir were discovered on east of China:**

- ◆ **CO<sub>2</sub> reservoir in Wanjinta of Songliao Basin**
- ◆ **Huanghua Depression Basin**
- ◆ **Jiyang Depression Basin**
- ◆ **Huangqiao CO<sub>2</sub> reservoir on the north of Jiangsu Province**
- ◆ **Sanshui Basin in Guangdong Province**



# Solution IV

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## Utilization of CO<sub>2</sub> venting in petrochemical industry:

Hydrogen technique: quantity of CO<sub>2</sub> venting is about  $6.65 \times 10^5$ t/a

Urea processing: quantity of CO<sub>2</sub> venting is about  $10^5$ t/a



# Concluding Remarks

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**CO<sub>2</sub> EOR technology has been paid more attention to in the world than before. Although there are some issues encountered on techniques, solutions have been put forward developing to CO<sub>2</sub> capture, storage and circulation for oil & gas development. Creating harmony of energy development and environment is inevitable trend for CO<sub>2</sub> EOR development.**



# Research on CO<sub>2</sub> EOR Technology and Application in China

